

Extended (Finite) Sources

Collimated X-ray

$$I_d(x_d, y_d) = I_0 \exp \left[- \int \mu_o(x, y, z) dz \right]$$

X-Ray with a Point Source

$$I_d(x_d, y_d) = I_i \exp \left[- \sqrt{1 + \frac{r_d^2}{d^2}} \int \mu_o \left(\frac{x_d}{d}z, \frac{y_d}{d}z, z \right) dz \right]$$

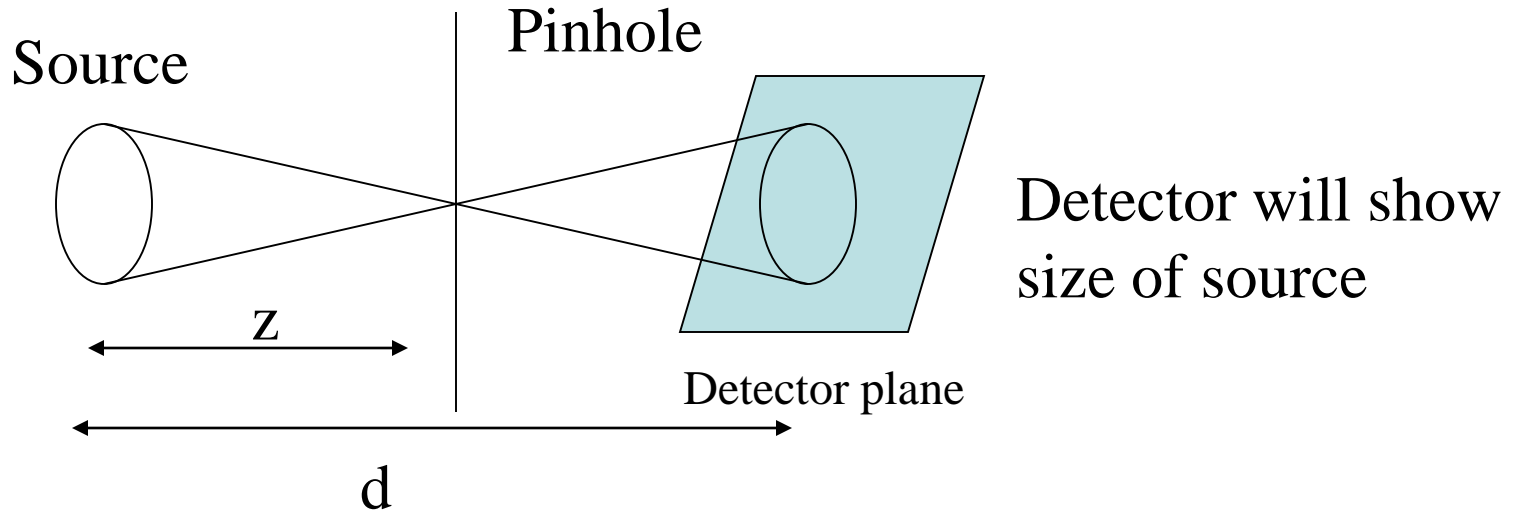
$$I_d(x_d, y_d) = I_i \exp \left[- \sqrt{1 + \frac{r_d^2}{d^2}} \int \mu_o \left(\frac{x_d}{M}, \frac{y_d}{M}, z \right) dz \right]$$

where $M = d/z$

and $I_i = I_0 / \left(1 + (r_d^2/d^2) \right)^{3/2}$

Finite source

Measuring Source Size



Place pinhole between source and detector. This pinhole reproduce an inverted image of source magnified by $(d-z)/z=m$.

The point response $h(x_d, y_d)$ for the pinhole for a source distribution $s(x_s, y_s)$ is:

$$h(x_d, y_d) = K_s s(x_s, y_s) = K_s s\left(\frac{x_d}{m}, \frac{y_d}{m}\right)$$

Finite source

The total detected Intensity (image) of a transparent object (hole) having transmission $t(x,y) = \exp [-\mu (x,y) \delta (z - z_0)]$ imaged by a finite x-ray source, $s(x,y)$ is obtained by convolution process:

$$I_d(x_d, y_d) = K t\left(\frac{x_d}{M}, \frac{y_d}{M}\right) ** s\left(\frac{x_d}{m}, \frac{y_d}{m}\right)$$

where: $M = \frac{d}{z}$ and $m = \frac{-(d-z)}{z}$

The detected image will be the convolution of a **M**agnified object and a **m**agnified source.

In frequency domain:

$$I_d(u, v) = KM^2 m^2 T(Mu, Mv) S(mu, mv)$$

Geometric Ray Optics

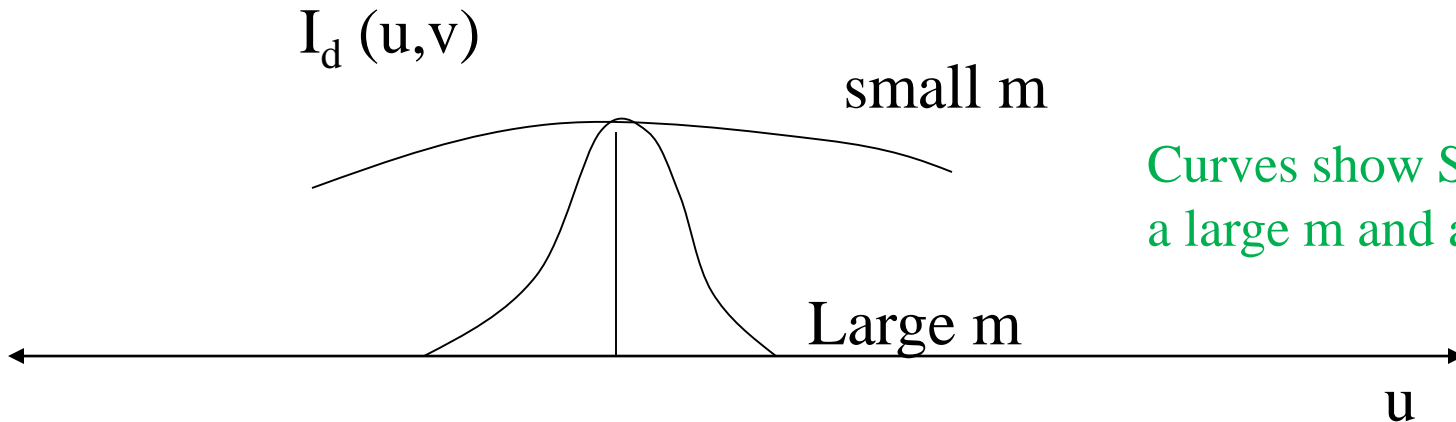
$$I_d(x_d, y_d) = Kt\left(\frac{x_d}{M}, \frac{y_d}{M}\right) ** s\left(\frac{x_d}{m}, \frac{y_d}{m}\right)$$

In the Fourier domain:

$$I_d(u, v) = KM^2m^2 T(Mu, Mv) S(mu, mv)$$

Object is magnified by $M=d/z$

Source magnification causes distortion: $m = \frac{-(d-z)}{z}$



Curves show $S(mu, mv)$ for a large m and a small m

Detailed Analysis

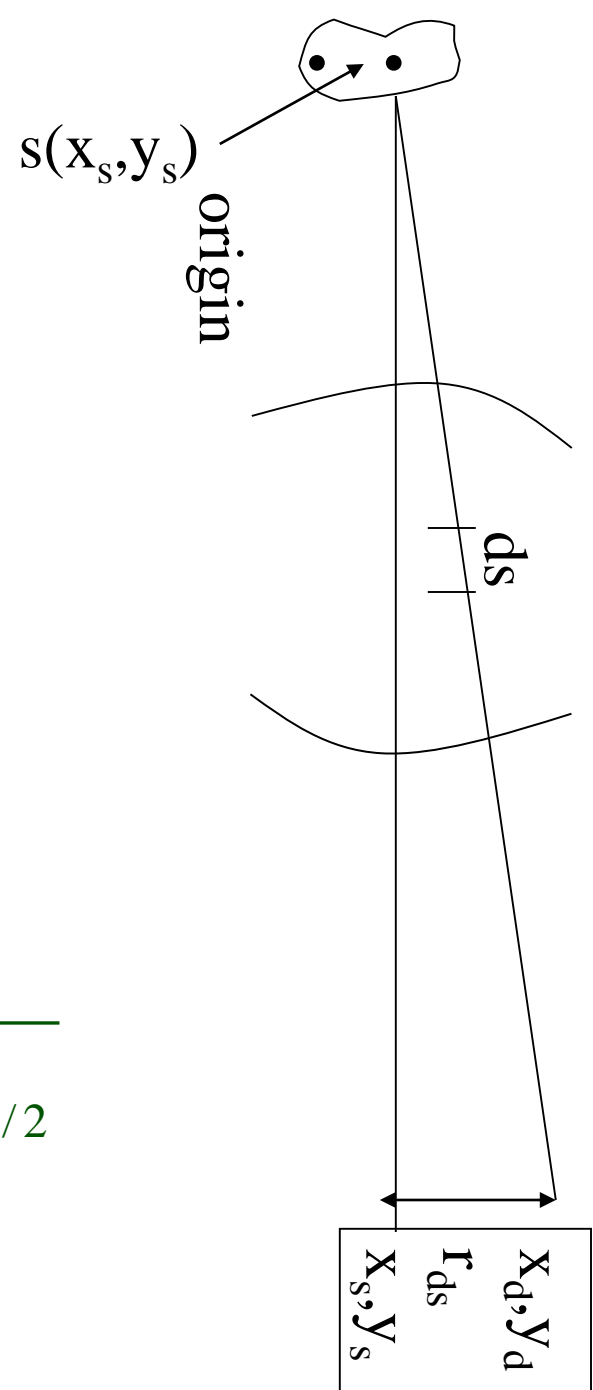
1) First, no object. Differential Intensity at detector plane:

$$dI_i(x_d, y_d) = dI_o \cos^3 \theta$$

$$dI_o = s(x_s, y_s) dx_s dy_s / (4\pi d^2)$$

Source units ((N/mm²)/min)

$$dI_d(x_d, y_d) = dI_o \frac{1}{\left(1 + \frac{r_d^2}{d^2}\right)^{3/2}}$$



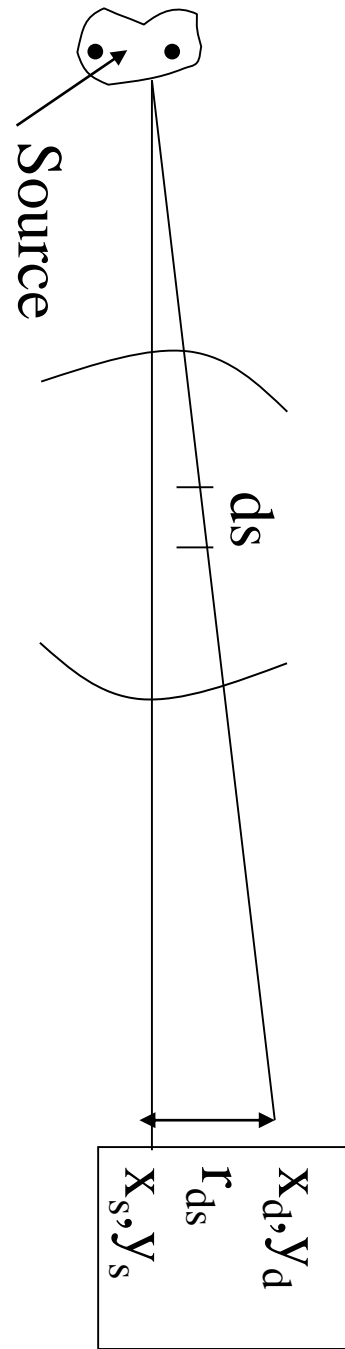
2) Now let's put in an object (for **object obliquity**).
 What is the output of x_d, y_d given a source at x_s, y_s ?

We call this the differential detected image.

$$dI_d(x_d, y_d, x_s, y_s) = dI_i \exp \left[- \int \mu(x, y, z) ds \right]$$

As before, we will evaluate ds in terms of x_d, y_d
 in the detector plane.

$$\begin{aligned} ds &= \sqrt{dx^2 + dy^2 + dz^2} \\ &= dz \sqrt{1 + (dx/dz)^2 + (dy/dz)^2} \end{aligned}$$



Now finding expressions for x and y paths in terms of z .

We want to describe what is happening at some general location x, y in the body.

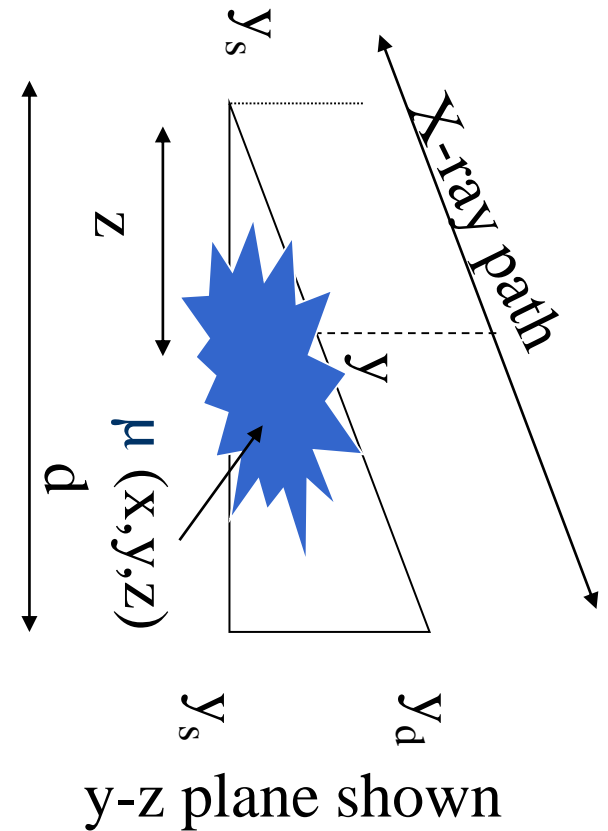
By similar triangles:

$$\frac{y_d - y_s}{y - y_s} = \frac{d}{z}$$

$$y_d - y_s \frac{z}{d} = y - y_s$$

$$y = \frac{((y_d - y_s)z)}{d} + y_s$$

Similarly $x = \frac{((x_d - x_s)z)}{d} + x_s$



Again, we will build a parametric equation

$$\frac{dx}{dz} = \frac{(x_d - x_s)}{d} \quad \frac{dy}{dz} = \frac{(y_d - y_s)}{d}$$

$$ds = \sqrt{dx^2 + dy^2 + dz^2} = dz \sqrt{1 + (dx/dz)^2 + (dy/dz)^2}$$

$$ds = dz \sqrt{1 + \left(\frac{x_d - x_s}{d}\right)^2 + \left(\frac{y_d - y_s}{d}\right)^2} = dz \sqrt{1 + \frac{r_d^2}{d^2}}$$

$$dI_d = dI_i \exp \left[-\sqrt{1 + \frac{r_d^2}{d^2}} \int \mu_m \left(\frac{x_d - x_s}{d} z + x_s, \frac{y_d - y_s}{d} z + y_s, z \right) dz \right]$$

Recalling that $M = \frac{d}{z}$ and $m = \frac{-(d-z)}{z}$

We can have the result at an arbitrary detector point and arbitrary source point.

$$dI_d = dI_i \exp\left[-\sqrt{1 + \frac{r_d^2}{d^2}} \int \mu_m\left(\frac{x_d - mx_s}{M}, \frac{y_d - my_s}{M}, z\right) dz\right]$$

To get the entire result $I_d(x_d, y_d)$, we add up the response from all the source points by integrating over the source.

$$I_d(x_d, y_d) = \iint dI_d(x_d, y_d, x_s, y_s) =$$

$$\frac{1}{4\pi d^2} \iint \frac{s(x_s, y_s)}{(1 + r_d^2 / d^2)^{3/2}} \exp\left[-\sqrt{1 + \frac{r_d^2}{d^2}} \int \mu_m\left(\frac{x_d - mx_s}{M}, \frac{y_d - my_s}{M}, z\right) dz\right] dx_s dy_s$$

Let's make some assumptions and simplify

1) Ignore both obliquity factors

2) Assume thin planar object at $z=z_0$ $\mu = \tau(x,y) \delta(z - z_0)$

$$I_d(x_d, y_d) = \frac{1}{4\pi d^2} \iint s(x_s, y_s) \exp\left[-\tau\left(\frac{x_d - mx_s}{M}, \frac{y_d - my_s}{M}\right)\right] dx_s dy_s$$

To define this expression in a space invariant convolution form, let:

$$x'_s = mx_s \quad \text{and} \quad y'_s = my_s$$

And by considering a magnified source and Magnified object, we can get space invariance as:

$$I_d = \frac{1}{4\pi d^2 m^2} \iint s\left(\frac{x'_s}{m}, \frac{y'_s}{m}\right) \exp\left[-\tau\left(\frac{x_d - x'_s}{M}, \frac{y_d - y'_s}{M}\right)\right] dx'_s dy'_s$$

or:

$$I_d = \frac{1}{4\pi d^2 m^2} s\left(\frac{x_d}{m}, \frac{y_d}{m}\right) ** \exp\left[-\tau\left(\frac{x_d}{M}, \frac{y_d}{M}\right)\right]$$

Let's make above expression linear by replacing:

$$t(x, y) = \exp[-\tau(x, y)]$$

Then:

$$I_d = \frac{1}{4\pi d^2 m^2} s\left(\frac{x_d}{m}, \frac{y_d}{m}\right) * * t\left(\frac{x_d}{M}, \frac{y_d}{M}\right)$$

Here the collection efficiency of pinhole is divided by the ratio of image and source area i.e. m_2

Consider 10mm object

1mm source

z	$ m $	M	Image size	Blur
d	0	1	10mm	0
$d/2$	1	2	20mm	1mm
$d/10$	9	10	100mm	9mm

Volumetric Object

What about volumetric objects? Ignoring obliquity, for thin plane we have:

$$I_d = \frac{1}{4\pi d^2 m^2} \iint s(x_s, y_s) \exp\left[-\tau\left(\frac{x_d - mx_s}{M}, \frac{y_d - my_s}{M}\right)\right] dx_s dy_s$$

Let's model object as an array of planes (|||||) $\tau(x, y)$

Therefore: $\mu = \sum_i \tau_i(x, y) \delta(z - z_i)$

where $m = m(z)$ or $m_i = -(d - z_i)/z_i$ and $M_i = d/z_i$

$$\exp\left[-\tau\left(\frac{x_d - mx_s}{M}, \frac{y_d - my_s}{M}\right)\right] \quad \text{term is still not linear however}$$

Let's assume the solid object as: $\int \mu dz = \sum \tau_i \ll 1$

Then we can linearize the exponent $\exp(-\sum \tau_i) = 1 - \sum \tau_i$

$$I_d = \frac{1}{4\pi d^2 m^2} \iint s(x_s, y_s) \left[1 - \sum \tau_i \left(\frac{x_d - m_i x_s}{M_i}, \frac{y_d - m_i y_s}{M_i}\right)\right]$$

$$I_d \approx I_i - \sum_i \frac{1}{(4\pi d^2 m_i^2)} s(x_d/m_i, y_d/m_i) \tau_i(x_d/M_i, y_d/M_i)$$

$$\text{where } I_i = \frac{1}{(4\pi d^2)} \iint s(x_s, y_s) dx_s dy_s$$

The output is seen as **incident radiation minus a summation of convolutions**. Good math, but poor approximation. This is true only in very thin regions of the body

Reasonable approximation (except at boundaries μ approaches 0)
 Where μ of water is considered as mean μ , and departure from that is μ_{Δ}

$$\mu = \mu_{\text{mean}} + \mu_{\Delta}$$

$$\exp [-\int(\mu_m + \mu_{\Delta}) dz] = \exp [-\int\mu_m dz] \exp [-\int\mu_{\Delta} dz]$$

Since $\int\mu_{\Delta} dz \ll 1$ We can linearize with the approximation
 $\approx [\exp -\int\mu_m dz] [1 - \int\mu_{\Delta} dz]$

$$I_d = \frac{1}{4\pi d^2 m^2} \iint s(x_s, y_s) \exp \left[-\int \mu_m \left(\frac{x_d - mx_s}{M}, \frac{y_d - my_s}{M}, z \right) dz \right] \times \\ \left[1 - \int \mu_{\Delta} \left(\frac{x_d - mx_s}{M}, \frac{y_d - my_s}{M}, z \right) dx_s dy_s \right]$$

Since μ_m is a constant, the first exponential term is a constant.

Since μ_m is a constant, we can make the approximation:

$$\mu_m \left(\frac{x_d - mx_s}{M}, \frac{y_d - my_s}{M}, z \right) \cong \mu_m \left(\frac{x_d}{M}, \frac{y_d}{M}, z \right)$$

The remaining integration can now be seen as a series of thin planes.

$$I_d = \left[\exp - \int \mu_m (x_d/M, y_d/M, z) dz \right] \cdot \left[I_i - \sum 1/(4\pi d^2 m_i^2) s (x_d/m_i, y_d/m_i) ** \tau_{\Delta i} (x_d/M_i, y_d/M_i) \right]$$

$$I_d = T_{\text{water}} (x_d, y_d) \left[I_i - \sum 1/(4\pi d^2 m_i^2) \cdot s ((x_d/m_i), (y_d/m_i)) ** \tau_{\Delta i} (x_d/M_i, y_d/M_i) \right]$$

where $T_{\text{water}} = \left[\exp - \int \mu_m (x_d/M, y_d/M, z) dz \right]$

and $I_i = 1/(4\pi d^2) \iint s(x_s, y_s) dx_s dy_s$

Thus, we have justified viewing the body as an array of planes.